

About interconnections of chemostats

Alain Rapaport

Team MODEMIC

UMR MISTEA - Montpellier

An initial framework

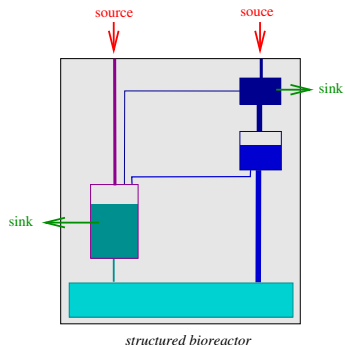
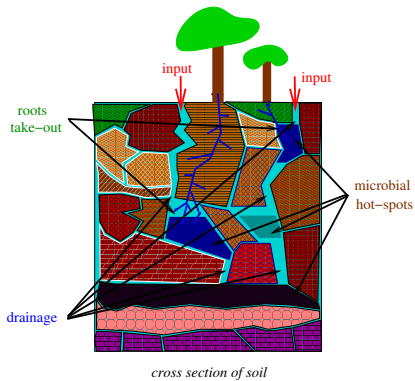
The ARC INRIA / AIP INRA **VITELBIO** 2009-10
(Virtual TELLuric BIOreactors)

Objective : study simple spatial representations of soil as a structured fermentor.




Main participants : UMR EcoSols (Montpellier), UMR Géosciences (Univ. Rennes 1), UREP (INRA Theix), ITK.

Web site : <https://sites.google.com/site/vitelbio/>

The VITELBIO project



The VITELBIO project

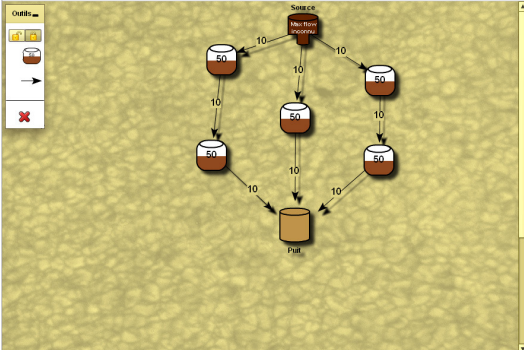
Vitelbio   

02_complex

4 Lancer une simulation avec le solveur Euler Leoda 5 Résultat

1 Réseau

Outils



```
graph TD; Source[Source] -- 10 --> N1((50)); Source -- 10 --> N2((50)); Source -- 10 --> N3((50)); N1 -- 10 --> N4((50)); N1 -- 10 --> N5((50)); N2 -- 10 --> N4; N2 -- 10 --> N5; N3 -- 10 --> N6((50)); N3 -- 10 --> N7((50)); N4 -- 10 --> Puit[Puit]; N5 -- 10 --> Puit; N6 -- 10 --> Puit; N7 -- 10 --> Puit;
```

2 Biologie

Paramètres des espèces

Tout cocher

| Modèle | Nom | K | Ki | Mu ma |
|----------------------------------|----------|---|----|-------|
| <input type="checkbox"/> Monod | Espèce 0 | 1 | 1 | 5 |
| <input type="checkbox"/> Haldane | Espèce 1 | 2 | 1 | 5 |

Visualiser les courbes de croissance

3 Concentration

Source 10 de substrat

| Chemostat | Substrat | Espèce 0 | Espèce 1 |
|-------------|----------|----------|----------|
| Chemostat 1 | 50 | 0 | 20 |
| Chemostat 2 | 0 | 15 | 20 |
| Chemostat 3 | 0 | 5 | 20 |
| Chemostat 4 | 10 | 0 | 20 |
| Chemostat 5 | 0 | 10 | 20 |

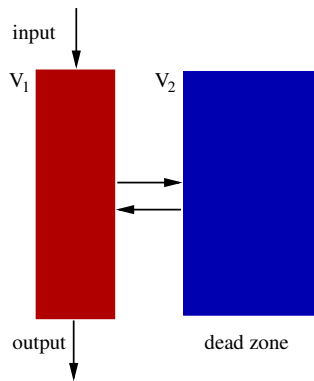
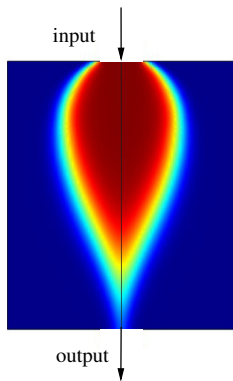
Main studies

- ▶ Effects of spatial structure and diffusion on the performances of the chemostat
 - ▶ co-supervision of a PhD student with UMR EcoSols
- ▶ About the benefit of the buffered chemostat
 - ▶ properties discovered thanks to simulations
- ▶ About niches and overyielding
 - ▶ primary work on the two species case
 - ▶ a lot remain to be done and understood...

Present and future directions

- ▶ **Waste water treatment in natural environments**
within associated team with Chile
collaboration with MOISE team
- ▶ **Input-output equivalence of hydric systems**
automatic control viewpoint
collaboration with GéoSciences Rennes

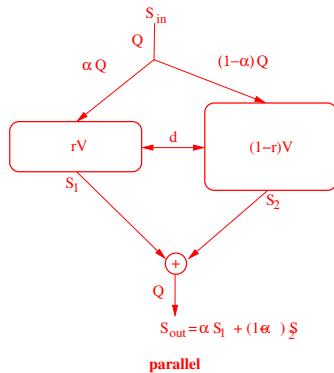
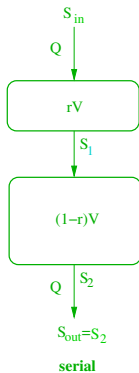
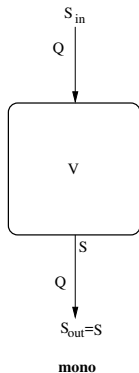
The spirit



Effects of spatial structure and diffusion on the performances of the chemostat

Participants : F. Gérard, I. Haidar, A. Rapaport.

Study of interconnected chemostats



The role of spatial structure

Proposition. For any monotonic increasing $\mu(\cdot)$, there exists a threshold \bar{s}_{in} such that

- ▶ $s_{in} > \bar{s}_{in}$, there exists a serial configuration s.t.

$$s_{out}^*(\text{serial}) < s_{out}^*(\text{mono}) < s_{out}^*(\text{parallel})$$

for any parallel configuration,

- ▶ $s_{in} < \bar{s}_{in}$, there exists a parallel configuration s.t.

$$s_{out}^*(\text{parallel}) < s_{out}^*(\text{mono}) < s_{out}^*(\text{serial})$$

for any serial configuration.

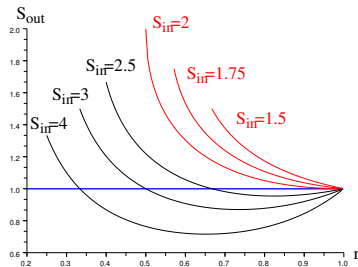
The role of diffusion

Proposition. For any monotonic increasing $\mu(\cdot)$, the parallel configuration satisfies the properties

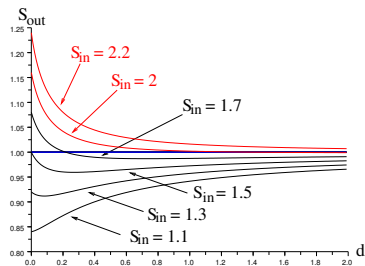
- ▶ $s_{in} > \bar{s}_{in}$, the map $d \mapsto s_{out}^*(d)$ is **decreasing**,
- ▶ $s_{in} < \bar{s}_{in}$, the map $d \mapsto s_{out}^*(d)$ admits an **unique minimum** for $d^* < +\infty$.

Furthermore, there exists another threshold $\underline{s}_{in} < \bar{s}_{in}$ s.t.
 $d^* = 0$ for $s_{in} < \underline{s}_{in}$.

Comparison of performances



serial



parallel

About the benefit of the buffered chemostat

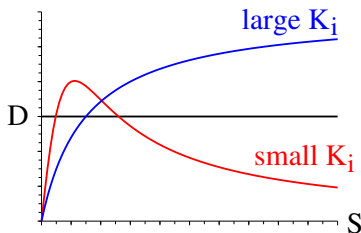
Participants : I. Haidar, J. Harmand, A. Rapaport.

The chemostat with inhibited growth

$$\begin{aligned}\dot{s} &= -\mu(s)x + D(s_{in} - s) && \text{(substrate concentration)} \\ \dot{x} &= \mu(s)x - Dx && \text{(biomass concentration)}\end{aligned}$$

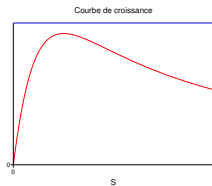
where $\mu(\cdot)$ is an **Haldane** function.

$$\mu(s) = \frac{\bar{\mu}s}{K + s + s^2/K_i}$$



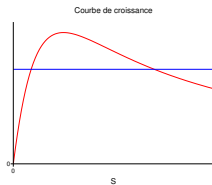
Example : J. F. Andrews, *A mathematical model for the continuous culture of microorganisms utilizing inhibitory substrates*, Biotech. Bioengr., 10 (1968), pp. 707-723.

Stability analysis for non-monotonic growth



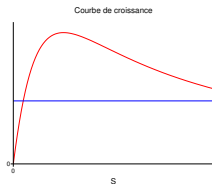
$$D > \max_{s \in [0, s_{in}]} \mu(s)$$

1 equilibrium : wash-out



$$\mu(s_{in}) < D < \max_{s \in [0, s_{in}]} \mu(s)$$

3 equilibria : bi-stability

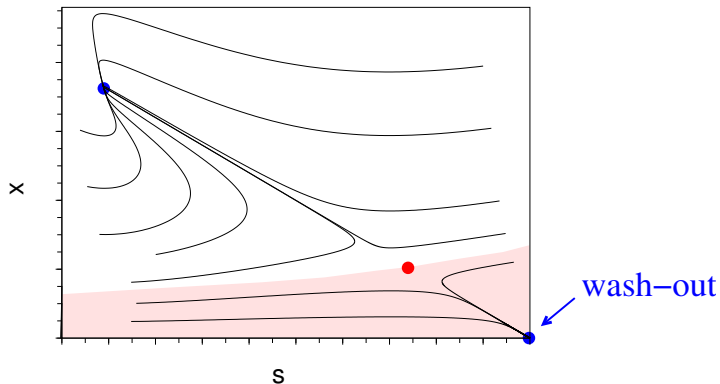


$$D < \mu(s_{in})$$

2 equilibria : stability

The bi-stability case

Under the condition $\mu(s_{in}) < D < \max_{s \in [0, s_{in}]} \mu(s)$



We are looking to ways to eliminate or reduce the attraction basin of the wash-out equilibrium

Solution A : feedback control

Example 1 : linearizing feedback control

$$D(s, x) = \frac{\mu(s)x - \lambda(s - s^*)}{s_{in} - s}$$

see Bastin Dochain 1986

Example 2 : P.I. controller

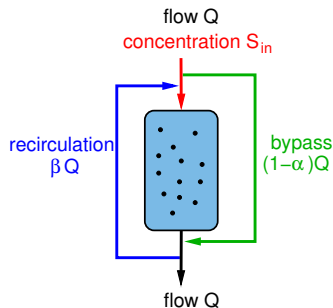
$$D(s) = G_1(s - s^*) + G_2 \int_0^t (s(\tau) - s^*) d\tau$$

see Shaum Alvarez Lopez-Arenas 2012

and many other contributors...

Drawback : requires an upstream tank while D is above its nominal value D^* , whose volume can be very large depending on the initial condition...

Solution B : re-circulation loops



D is fixed.

$$\text{Let } u = \frac{\alpha + \beta}{1 + \beta} \in [0, 1]$$

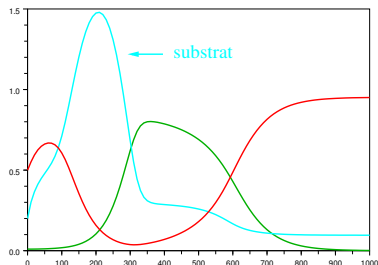
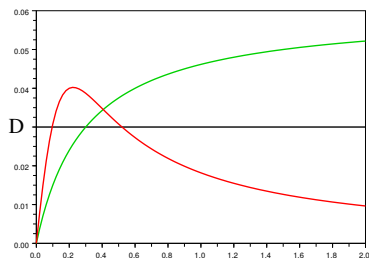
Proposition. See Harmand Mazenc R. 2004

$$u(s) = \begin{cases} \min\left(1, \frac{\mu(s) - \mu(s^*) + D}{D}\right) & \text{if } s > s^* \\ \frac{s_{in} - s^*}{s_{in} - s} & \text{if } s \leq s^* \end{cases}$$

G.A.S. the chemostat about $(s^*, s_{in} - s^*)$.

Drawback : In the transient, output s can be above s^* for a long time...

Solution C : the “bio-control”



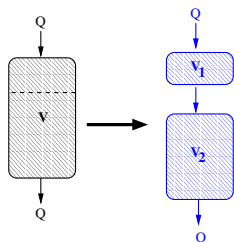
The presence of the “green” species at initial time allows a G.A.S. equilibrium with the “red” species (alone). See Harmand R. 2008.

Drawback : Requires to find and add the “good” species...

The role of spatialisation

Consider V and Q such that $\mu(s_{in}) < \frac{Q}{V} < \max_{s \in [0, S_{in}]} \mu(s)$.

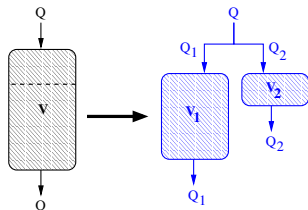
Serial structure with $V = V_1 + V_2$:



$$V_i < V \Rightarrow \frac{Q}{V_i} > \mu(s_{in}) \quad (i = 1, 2)$$

\Rightarrow both wash-out are attractive!

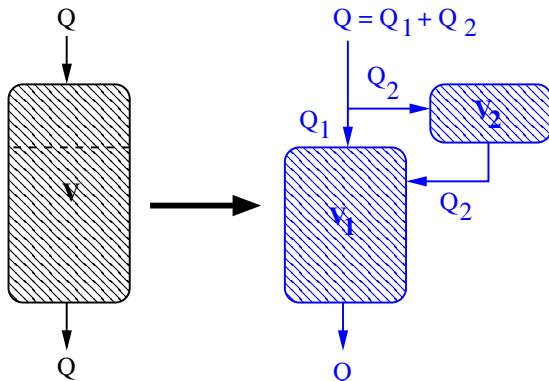
Parallel structure with $V = V_1 + V_2$ and $Q = Q_1 + Q_2$:



$$\frac{Q_i}{V_i} < \frac{Q}{V} \Rightarrow \frac{Q_j}{V_j} > \frac{Q}{V} \quad (i \neq j)$$

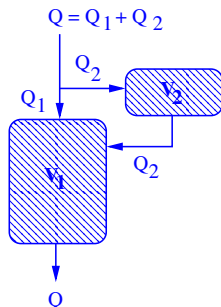
\Rightarrow at least one wash-out is attractive!

Solution D : the “buffered” chemostat



with $V = V_1 + V_2$

Solution D : the “buffered” chemostat



Two degrees of freedom : (α, r) with

$$\frac{Q_2}{V_2} = \alpha D \text{ and } V_1 = rV$$

- ▶ *buffer tank* : the classical chemostat model
⇒ unique positive eq. $s_2^*(\alpha)$ if $\alpha D < \mu(s_{in})$
- ▶ *main tank* : chemostat with two inputs :

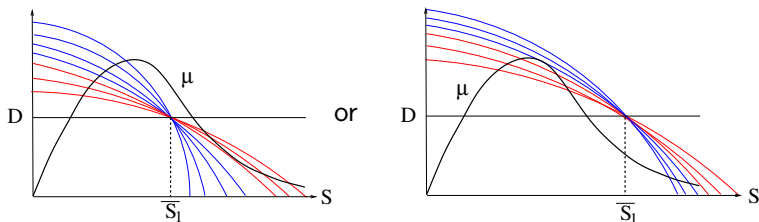
$$\mu(s_1^*) = \frac{D}{r} - \alpha D \left(1 - \frac{1}{r}\right) \frac{s_{in} - s_2^*(\alpha)}{s_{in} - s_1^*} = \phi_{\alpha,r}(s_1^*)$$

Solution D : the “buffered” chemostat

Proposition. See Haidar R. Harmand 2013

For any $\alpha \in (0, \mu(s_{in}))$, there exists $\bar{r}(\alpha) \in (0, 1)$ such that

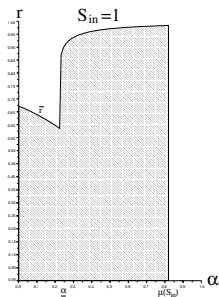
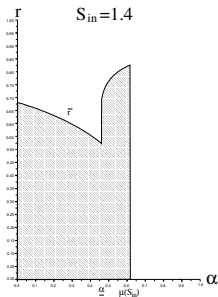
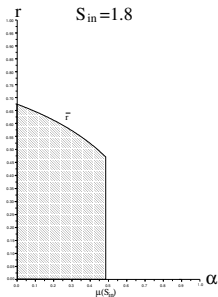
- ▶ for any $r < \bar{r}(\alpha)$, the dynamics admits an **unique positive equilibrium**,
- ▶ for any $r > \bar{r}(\alpha)$, the dynamics admits at least three positive equilibrium.



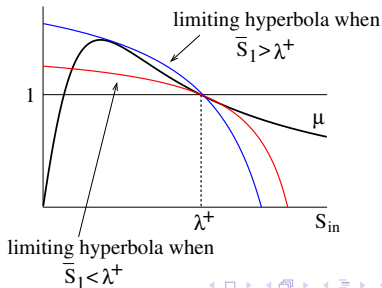
where $\bar{S}_1 = \alpha s_2^*(\alpha) + (1 - \alpha)s_{in}$ fulfills $\phi_{\alpha,r}(\bar{S}_1) = 1, \forall r$

The set of G.A.S. configurations

Examples with the Haldane law and $D = 1$:



Limiting cases : $\bar{s}_1 = \lambda^+$



Performances of the “buffered” chemostat

Consider $\psi(s) = \mu(s)(S_{in} - s)$

Let $\psi^* = \max_{s \in [0, \bar{s}]} \psi(s)$ where $\mu(\bar{s}) = \mu(s_{in})$.

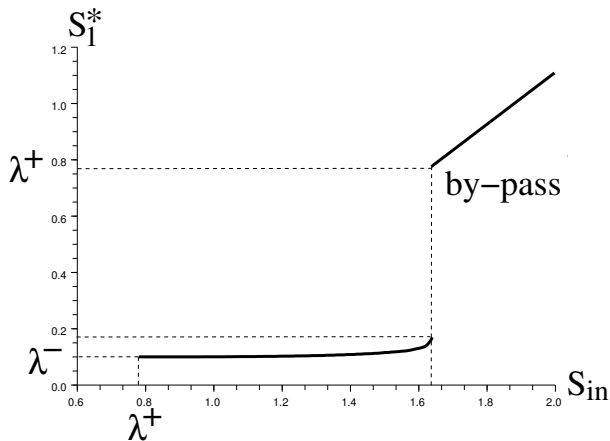
Let $s^* \in \arg \max \psi^*$ and define $\alpha^* = \mu(s^*)$.

Proposition. See Haidar R. Harmand 2013

The best stable configuration consists in having $\alpha = \alpha^*$ and

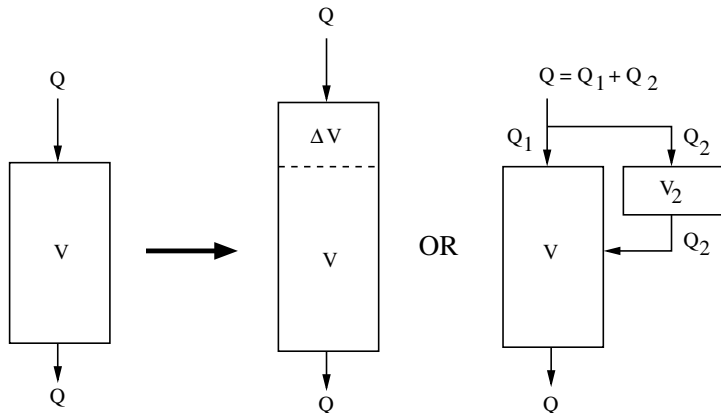
- ▶ making a **by-pass** of the volume V with a flow rate equal to $(1 - \alpha^*)Q$, when $\psi^* < S_{in} - \lambda_+$.
- ▶ choosing any value of $r \in (0, \bar{r}(\alpha^*))$, when $\psi^* = S_{in} - \lambda_+$.
- ▶ taking r smaller and arbitrarily close to $\bar{r}(\alpha^*)$, when $\psi^* > S_{in} - \lambda_+$.

Performances of the “buffered” chemostat



smallest output concentration at steady state
as function of S_{in}

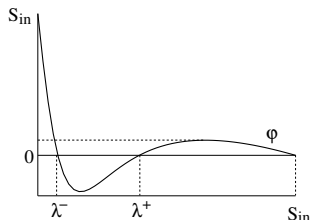
Adding a “buffer”



What is the smallest volume to add to obtain global stability?

The “buffered” interconnection

Let $\varphi(s) = (s_{in} - s)(D - \mu(s))$



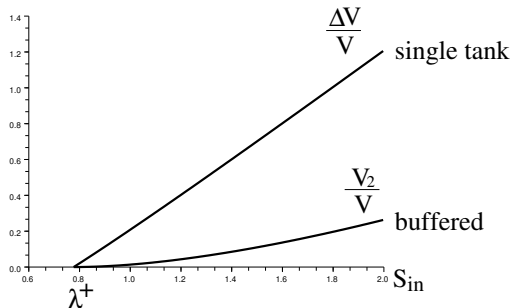
Proposition. See Haidar R. Harmand 2013.

The G.A.S. property is fulfilled for an additional volume such that

$$V_2 > \frac{V}{\psi^*} \max_{s \in (\lambda^+, s_{in})} \varphi(s)$$

Comparison with a single tank

For a single tank, one should have $\Delta V > V \left(\frac{1}{\mu(s_{in})} - 1 \right)$.



Main messages

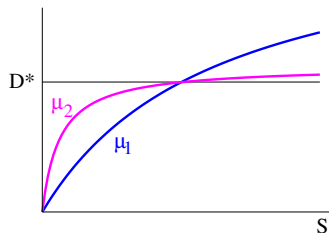
- ▶ A buffered interconnection of two volumes can globally stabilize the chemostat, preserving the total volume and input rate (while this is not possible with serial or parallel interconnections).
- ▶ We have characterized the set \mathcal{C} of such configurations and among them the one that presents the best conversion.
- ▶ The input concentration impacts the shape of \mathcal{C} . There exists a threshold above it a by-pass is more efficient.
- ▶ The minimum volume to add to a given single tank for obtaining the global stability can be significantly reduced using a “buffered” interconnection.

About niches and overyielding

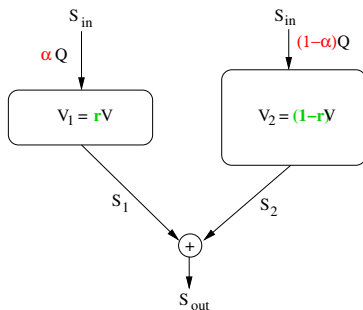
Participants : D. Dochain, P. de Leenheer, A. Rapaport.

Two species two habitats

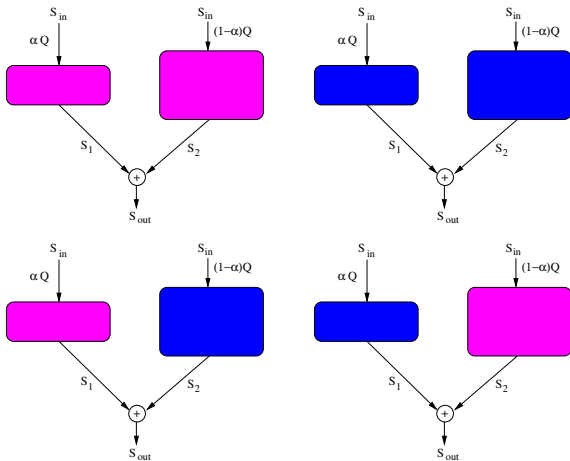
Consider two species



and a spatial structure



Bioconversion overyielding



Which is the best configuration ?

Steady state overyielding

Assumption : $\mu(\cdot)$ is increasing.

$$\text{Let } \lambda(D) = \begin{cases} \mu^{-1}(D) & \text{if } D \leq \mu(s_{in}) \\ s_{in} & \text{if } D > \mu(s_{in}) \end{cases}$$

Define $F(\alpha, r) := \alpha \lambda\left(\frac{\alpha}{r} D\right) + (1 - \alpha) \lambda\left(\frac{1 - \alpha}{1 - r} D\right)$

Definition : There is **overyielding** exactly when

$$G(\alpha, r) := \alpha \lambda_1\left(\frac{\alpha}{r} D\right) + (1 - \alpha) \lambda_2\left(\frac{1 - \alpha}{1 - r} D\right) < \min(F_1(\alpha, r), F_2(\alpha, r))$$

Steady state overyielding

$$C = \{(\alpha, r) \in [0, 1]^2 \mid (\alpha/r)D \leq \mu(s_{in}) \text{ and } ((1 - \alpha)/(1 - r))D \leq \mu(s_{in})\}$$

$$T_1 = \{(\alpha, r) \in [0, 1]^2 \mid (\alpha/r)D > \mu(s_{in})\}$$

$$T_2 = \{(\alpha, r) \in [0, 1]^2 \mid ((1 - \alpha)/(1 - r))D > \mu(s_{in})\}$$

Proposition. If $\mu(\cdot)$ is concave then the restriction of F on C is convex.

Proposition. Define $T^{in}(D) = \lambda(D) + D\lambda'(D)$. One has

$$\min_{[0,1]^2} F = \begin{cases} \lambda(D) = F(\alpha, \alpha), \forall \alpha \in [0, 1], \text{ for } s_{in} \geq T^{in}(D) \\ \min_{\alpha} F(\alpha, 0) < \lambda(D), \text{ for } s_{in} < T^{in}(D) \end{cases}$$

Steady state overyielding

Assume that there exists D^* such that $\lambda_1(D^*) = \lambda_2(D^*)$.

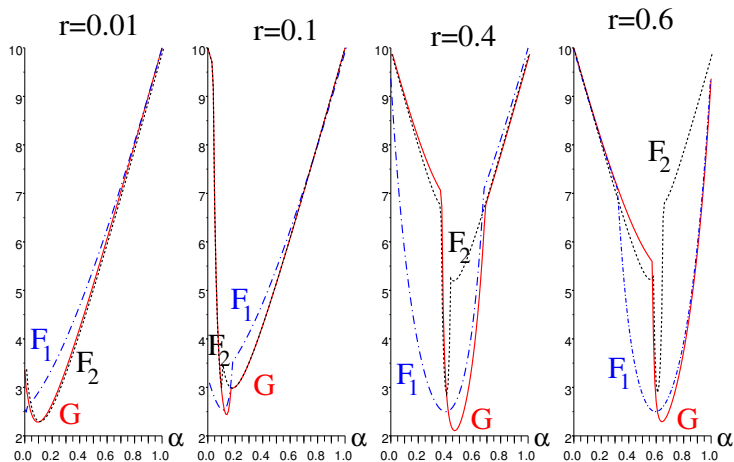
Proposition. When $D = D^*$ and $\alpha \in (0, 1)$, there exist configurations close to (α, α) that present overyielding.

Proposition. When $D \neq D^*$, there exists (α, r) with

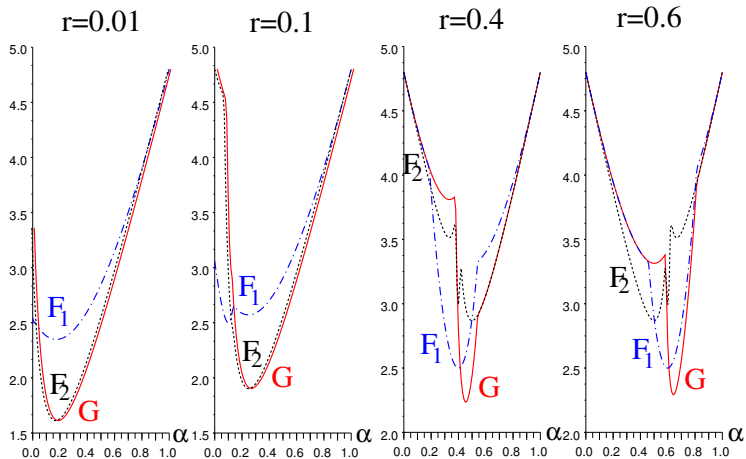
$$\frac{\alpha}{r}D < D^* < \frac{1-\alpha}{1-r}D < \min(\mu_1(s_{in}), \mu_2(s_{in}))$$

that corresponds to overyielding.

Example (large s_{in})



Example (small s_{in})

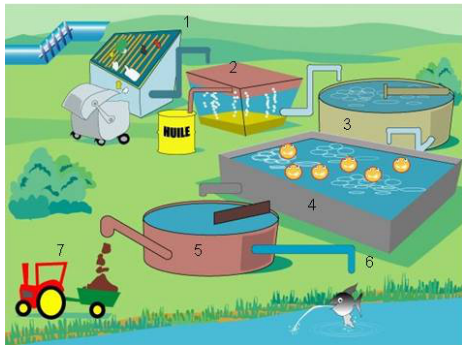


Waste water treatment in natural environments

Participants : P. Gajardo, J. Harmand, A. Rapaport, H. Ramirez,
V. Riquelme, A. Rousseau.

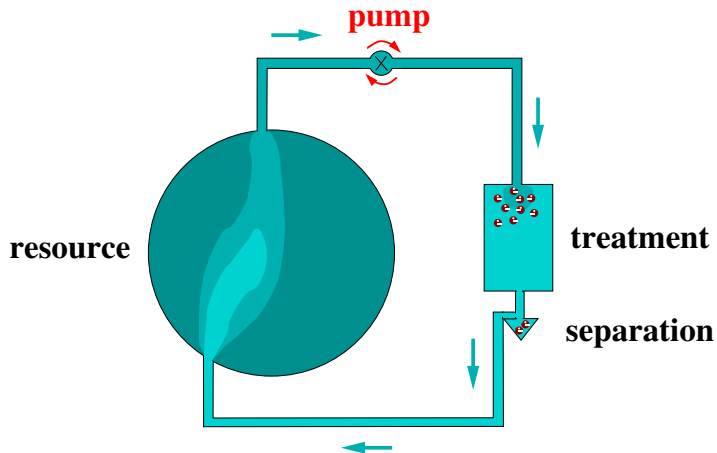
Industrial or municipal waste treatment

waste
→



discharge
→

Closed circuit treatment

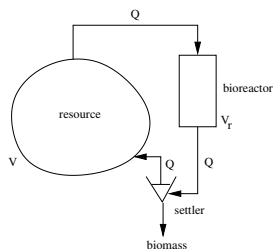


The control problem

Objective : clean up in minimal time .

- ▶ which information on the parameters of the model are useful for reaching the target in minimal time ?
- ▶ could it be better operating a non-constant flow Q ?
- ▶ which variable(s) have to be measured on-line ?
- ▶ what is the influence of an **inhomogeneity** of the substrate concentration of the resource ?

The homogeneous case



$$\begin{aligned}\dot{S} &= \frac{Q}{V}(S_r - S) \\ \dot{S}_r &= -\mu(S_r)X_r + \frac{Q}{V_r}(S - S_r) \\ \dot{X}_r &= \mu(S_r)X_r - \frac{Q}{V_r}X_r\end{aligned}$$

Target : $S \leq \underline{S}$

Hypotheses : $V \gg V_r$, $\mu(\cdot)$ increasing concave.

Slow-fast approximation :

$$\boxed{\mu(S_r(Q)) = \frac{Q}{V_r}} \Rightarrow \boxed{\dot{S} = \frac{Q}{V}(S_r(Q) - S)}$$

Optimization among feedbacks

Proposition. $Q^{opt}(S) = V_r \mu(S_r^{opt}(S))$ is an optimal feedback with

$$S_r^{opt}(S) \in \arg \max_{S_r \in (0, S)} \mu(S_r)(S - S_r)$$

- ▶ $\mu(\cdot)$ linear,

$$S_r^{opt}(S) = \frac{S}{2}$$

- ▶ $\mu(\cdot)$ Monod : $\mu(s) = \mu_{\max} \frac{s}{K + s}$

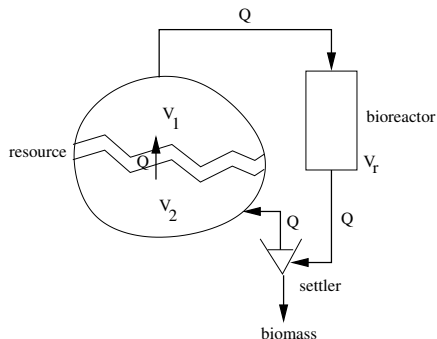
$$S_r^{opt}(S) = \sqrt{K^2 + KS} - K .$$

Numerical simulations

| μ_{\max} | K | V | V_r | $S(0)$ |
|--------------|-----|------|-------|--------|
| 1.0 | 1.0 | 1000 | 1 | 1 |

| \underline{S} | T_f^* | T_{opt} | gain |
|-----------------|---------|-----------|------|
| 0.5 | 5420 | 5293 | 1.9% |
| 0.4 | 8064 | 7719 | 3.7% |
| 0.3 | 12499 | 11606 | 7.2% |
| 0.2 | 21663 | 19062 | 12% |
| 0.1 | 51626 | 40425 | 22% |

Modelling the inhomogeneity



with $V = V_1 + V_2$
 $p = V_1/V_1$

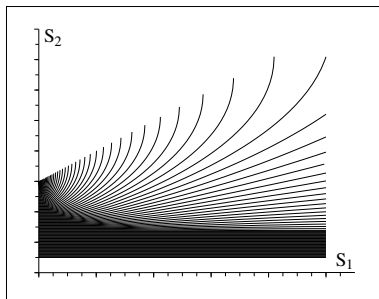
$$\begin{cases} \dot{S}_1 = \frac{Q}{V_1}(S_2 - S_1) = \mu(S_r) \frac{V_r}{V_1}(S_2 - S_1) \\ \dot{S}_2 = \frac{Q}{V_2}(S_r(Q) - S_2) = \mu(S_r) \frac{V_r}{V_2}(S_r - S_2) \end{cases}$$

$\mathcal{D} = \{(S_1, S_2) \in \mathbb{R}_+^2 \mid S_1 \geq S_2\}$ is invariant.

Optimization among feedbacks

Proposition. For any initial condition in \mathcal{D} , the optimal policy Q^{opt} consists in **two steps** :

1. (possibly void) a **non constant feedback** until S_2 reaches a value $\underline{S}_2 < \underline{S}_1$,
2. a **constant control** $Q^{opt} = V_r \mu(\underline{S}_2)$ until S_1 reaches \underline{S} .



Field of extremals

Numerical simulations

| | $p = 0$ | $p = 0.2$ | | | $p = 0.5$ | | |
|-----------------|---------|-----------|-----------|-----|-----------|-----------|-----|
| \underline{S} | T_f^* | T_f^* | T_{opt} | % | T_f^* | T_{opt} | % |
| 0.7 | 2387 | 2708 | 2661 | 1.7 | 2931 | 2881 | 1.7 |
| 0.6 | 3660 | 3816 | 3756 | 1.6 | 3993 | 3951 | 1.1 |
| 0.5 | 5420 | 5325 | 5194 | 2.5 | 5385 | 5317 | 1.2 |
| 0.4 | 8064 | 7567 | 7329 | 3.2 | 7395 | 7250 | 2.0 |
| 0.3 | 12499 | 11338 | 10754 | 5.4 | 10696 | 10320 | 3.6 |
| 0.2 | 21663 | 19137 | 17297 | 11 | 17389 | 16 180 | 7.4 |

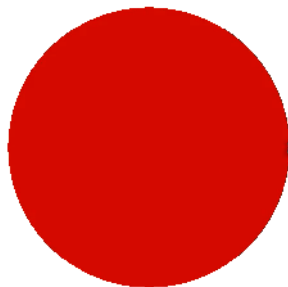
Facing realistic simulations

$$\begin{aligned}u_t + \mathbf{u} \cdot \nabla \mathbf{u} - \nu_u \Delta \mathbf{u} + \nabla p &= 0 \\ \nabla \cdot \mathbf{u} &= 0 \\ S_t + \mathbf{u} \nabla S - \nu_S \Delta S &= 0\end{aligned}$$

Boundary of the domain : $\Gamma = \Gamma_0 \cup \Gamma_{in} \cup \Gamma_{out}$

$$\begin{aligned}u &= 0, & x &\in \Gamma_0 \\ u \cdot n &= Qf(x), & u \cdot \tau &= 0, & x &\in \Gamma_{in} \cup \Gamma_{out} \\ \frac{\partial S}{\partial n} &= 0, & & & x &\in \Gamma_0 \cup \Gamma_{out} \\ S &= S_r(Q), & & & x &\in \Gamma_{in}\end{aligned}$$

Numerical simulation



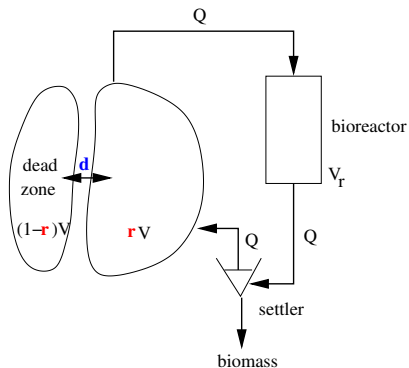
0.231

0.837

1

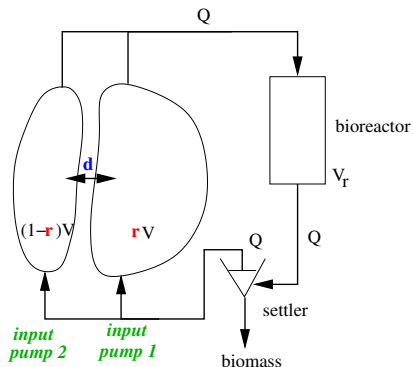


Consideration of a dead zone



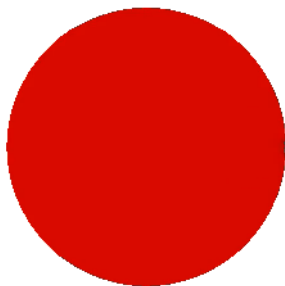
Proposition The same feedback as without dead zone is optimal, whatever are parameters r and d .

Multi-input pumps consideration



Proposition The optimal strategy consists in reaching $S_1 = S_2$ with only one input pump, and then to stay on the *singular arc* $S_1 = S_2$ using the two input pumps.

Multi-output pumps simulation



0.0%

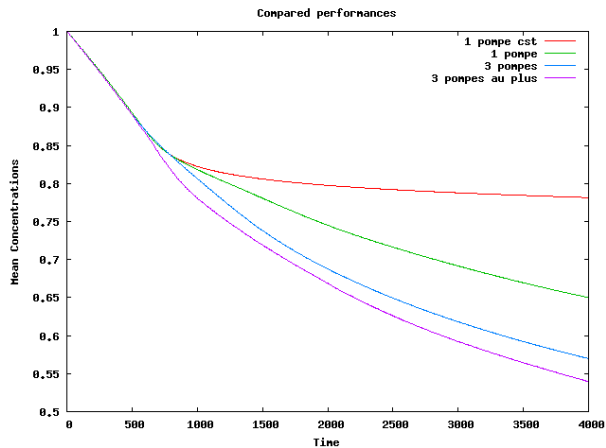
0.636

1.5



T
Δ %

Numerical comparison



Main messages

- ▶ A feedback strategy can significantly improve the total duration of treatment,
- ▶ A resource with an inhomogeneous concentration reduces the treatment duration under **large concentrations**,
- ▶ One needs to know the shape of the growth function to choose optimally the feedback.